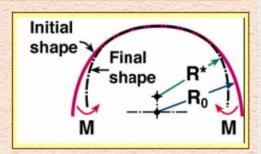
9 Curved Beams

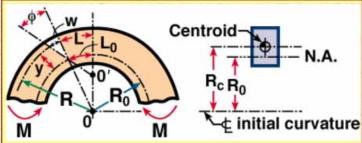
- 9.1 Definition
- 9.2 Differences Between Bending Behavior of a Straight and a Curved Beam
- 9.3 Pure Bending of Planar Curved Beams - Winkler Theory
- 9.4 Displacements of Curved Beams
- 9.5 Examples

Definition

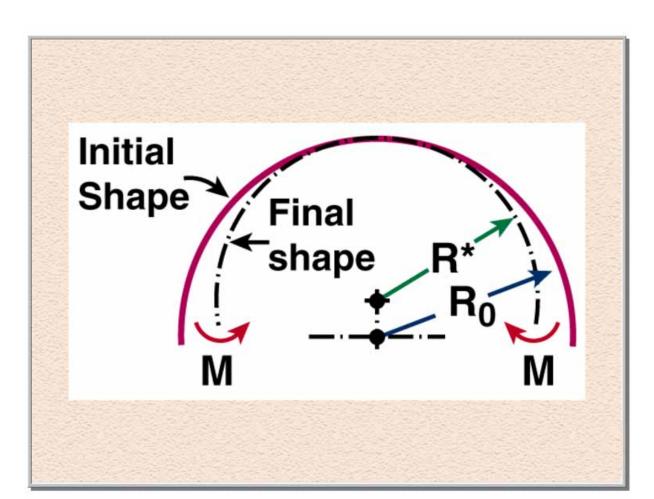
 A curved beam is a structural element for which the locus of the centroids of the cross sections is a curved line.

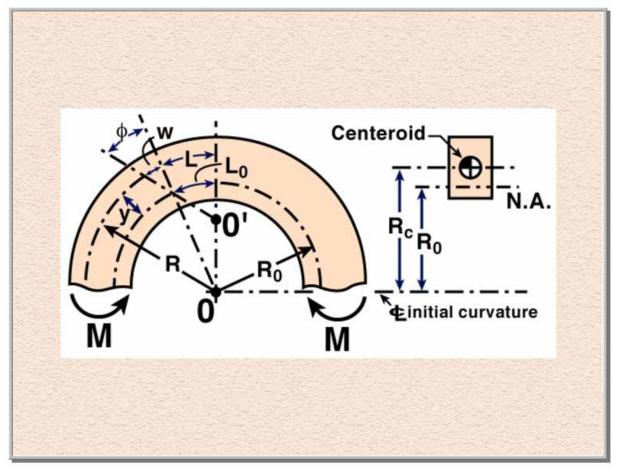


 When the radius of curvature is less than five times the cross sectional depth, the assumption of linear bending strain normal to the neutral axis



becomes inaccurate. However, the assumption of plane cross sections remain plane after bending is still valid.





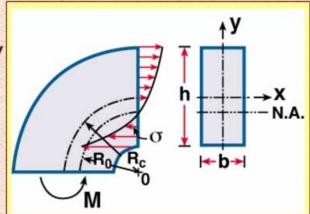
Differences Between Bending Behavior of a Straight and a Curved Beam

The assumption of plane cross sections remain plane results in linear strain distribution in straight beams, but not in curved beams.

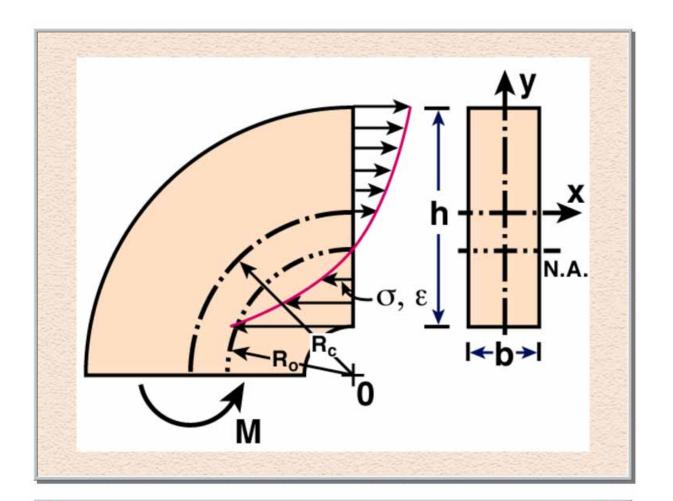
Pure Bending of Planar Curved Beams Winkler Theory

Basic Assumptions

- All cross sections possess a vertical axis of symmetry lying in the plane of the centroidal axis.
- The plane of bending coincides with the plane of symmetry of the beam.



 Plane cross sections before deformation remain plane after deformation.



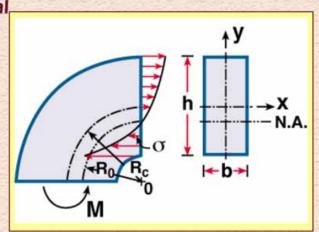
Kinematic Relations

R₀ = initial distance from the center of curvature to neutral axis (before deformation)

$$\frac{1}{R_0}$$
, $\frac{1}{R^*}$ = initial and final curvatures

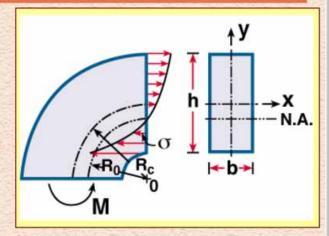
K = curvature change

$$=\frac{1}{R^*}-\frac{1}{R_0}$$



K = curvature change

$$=\frac{1}{R^*}-\frac{1}{R_0}$$



L₀ = distance measured along the neutral surface (as yet unknown)

W = axial displacement of a typical point distance y from the neutral axis

$$= y L_0 K$$

Pure Bending of Planar Curved Beams Winkler Theory

L₀ = distance measured along the neutral surface (as yet unknown)

w = axial displacement of a typical point distance y from the neutral axis

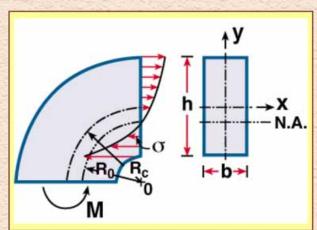
=
$$y L_0 K$$

E = axial strain

$$= y \frac{L_0}{L} \kappa$$

but

$$\frac{L_0}{R_0} = \frac{L}{R_0 + y}$$

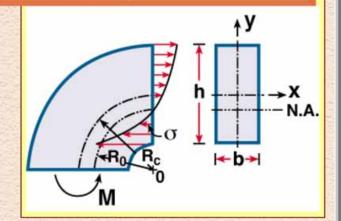


$$\varepsilon = \text{axial strain}$$

$$= y \frac{L_0}{L} \kappa$$

but

$$\frac{L_0}{R_0} = \frac{L}{R_0 + y}$$



where L = distance measured along a fiber distance y from the neutral axis

Therefore,
$$\varepsilon = y \frac{1}{1 + \frac{y}{R_0}} \kappa$$

i.e., the strain distribution in the y direction is hyperbolic.

Pure Bending of Planar Curved Beams Winkler Theory

Static Relations

$$N = \int_A \sigma dA = 0$$

$$M_x = \int_A \sigma y dA$$

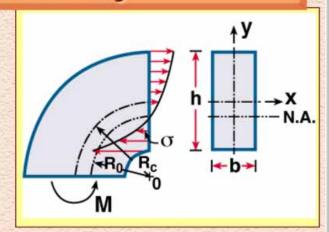
= M

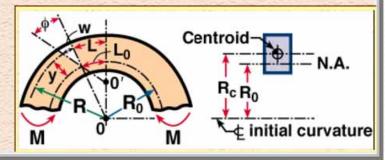
Constitutive Relations

for linearly elastic material

$$\sigma = E_{\varepsilon}$$

$$\sigma \Big|_{y} = E \frac{y}{1 + \frac{y}{R_{0}}} \kappa$$



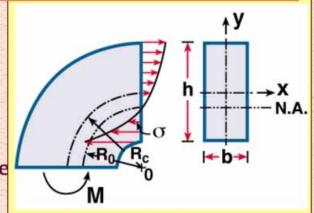


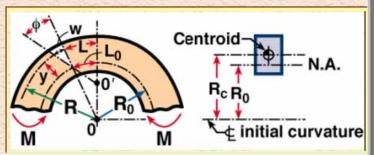
Constitutive Relations for linearly elastic material σ = Εε

$$\sigma \bigg|_{y} = E \frac{y}{1 + \frac{y}{R_0}} \kappa$$

This gives the location of the neutral axis, replacing y by its expression in terms of R

and R_0 . $y = R - R_0$





Pure Bending of Planar Curved Beams Winkler Theory

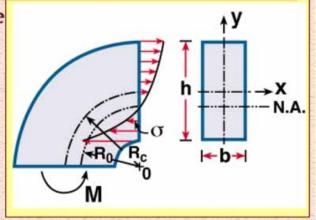
This gives the location of the neutral axis, replacing y by its expression in terms of R and R₀.

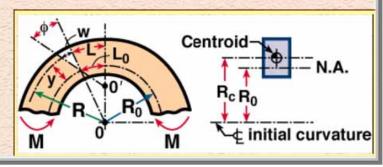
$$y = R - R_o$$

$$\int_A dA - R_0 \int_A \frac{dA}{R} = 0$$

or,

$$R_0 = \frac{A}{\int_A \frac{dA}{R}}$$





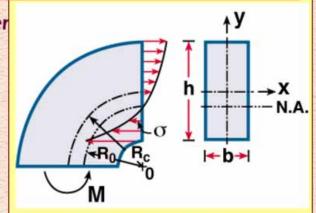
The neutral axis lies between the centoidal axis and the center of curvature.

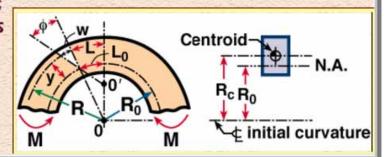
The quantity
$$\int_{A} \frac{dA}{R}$$
 is a

property of the cross sectional area

where \bar{y} = distance from the neutral axis to the centroidal axis

$$\sigma = \frac{M_x y}{A \bar{y} (R_0 + y)}$$



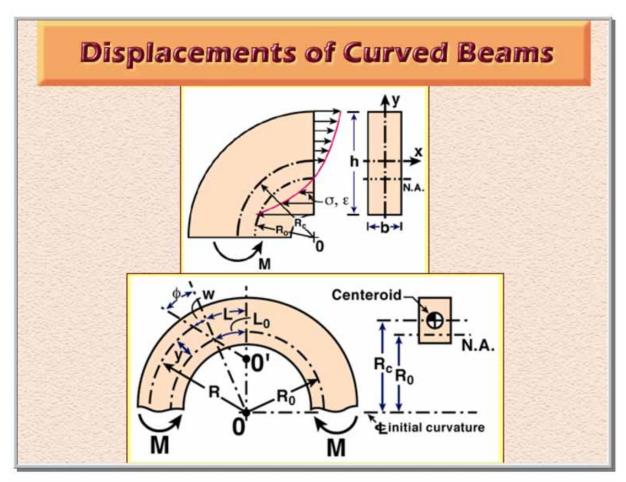


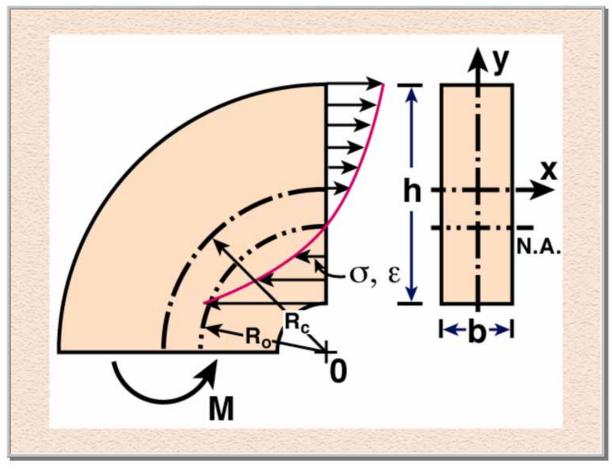
Pure Bending of Planar Curved Beams Winkler Theory

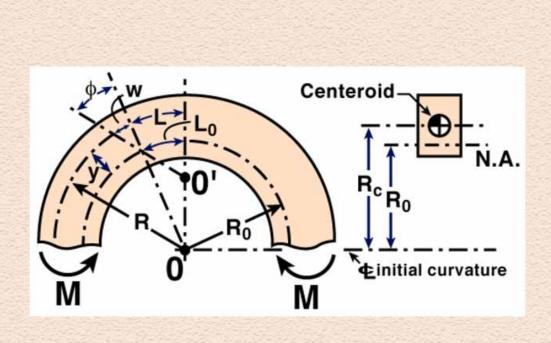
The stress distribution across the depth of the beam is hyperbolic. The maximum stress occurs at the outer fibers on the concave side of the beam.

Case of Combined Axial Force and Bending Moment

$$\sigma = \frac{N}{A} + \frac{M_x y}{A \bar{y} (R_0 + y)}$$







For a beam with a rectangular cross section, if the inside and outside radii are \mathbb{R}_1 and \mathbb{R}_2 , then

$$R_{0} = \frac{A}{\int_{A} \frac{dA}{R}}$$

$$= \frac{bh}{b \int_{R_{1}}^{R_{2}} \frac{dR}{R}}$$

$$= \frac{h}{\ln R_{2} - \ln R_{1}}$$
Centeroid

N.A.

$$R_{c}R_{0}$$

$$M$$
Centeroid

$$R_{c}R_{0}$$

$$M$$
M
Centeroid

$$R_{c}R_{0}$$

$$M$$
M
Centeroid

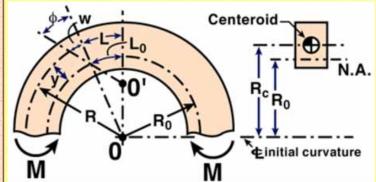
$$R_{c}R_{0}$$

$$M$$
M
Centeroid

$$R_{c}R_{0}$$

$$M$$
N.A.

$$= \frac{bh}{b \int_{R_1}^{R_2} \frac{dR}{R}}$$



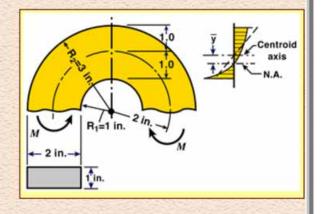
$$= \frac{h}{\ln R_2 - \ln R_1}$$

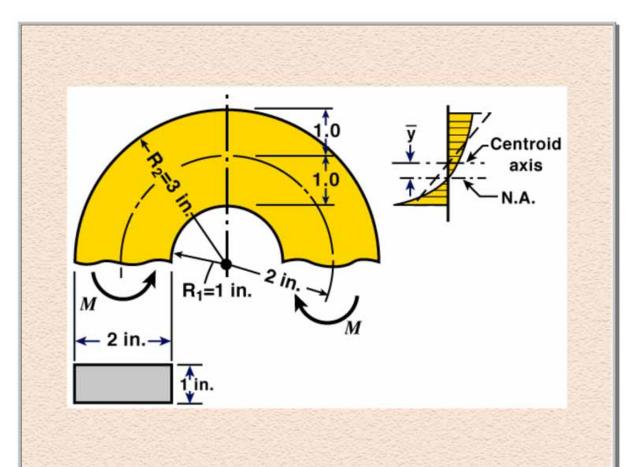
$$= \frac{h}{\ln \left(\frac{R_2}{R_1} \right)}$$

Displacements of Curved Beams

Comparison between maximum bending stresses in curved and straight beams

A = 2
$$R_0 = \frac{2}{\ln \frac{3}{1}}$$
= 1.82
$$\bar{y} = 0.18$$





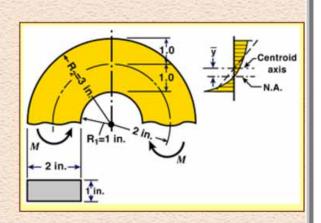
Maximum stresses occur on the inside surface

$$\sigma_{\text{max}} = \frac{M_{\text{x}} \ 0.82}{2 \times 0.18 \times 1}$$

= 2.28 M

For a straight beam

$$\sigma_{\text{max}} = 6 \frac{M}{\text{bh}^2}$$
$$= 1.5 \text{ M}$$



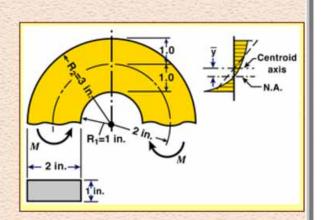
For a straight beam

$$\sigma_{\text{max}} = 6 \frac{M}{\text{bh}^2}$$

$$= 1.5 \text{ M}$$

$$k = \frac{\sigma_{\text{max}}}{\sigma_{\text{max}}} \frac{\sigma_{\text{curved}}}{\sigma_{\text{max}}}$$

$$= 1.52$$



Displacements of Curved Beams

